

1.29 SOLAR / 1018 - 19/02

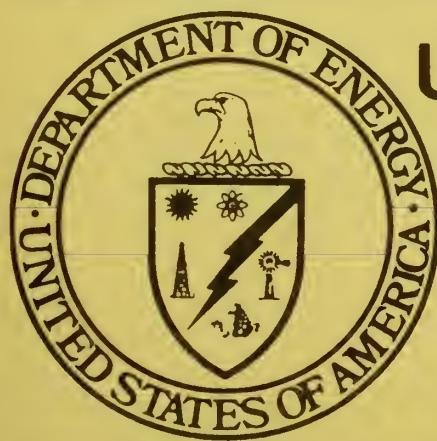
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SOLAR/1018-79/02

Monthly Performance Report

STEWART-TEELE-MITCHELL

FEBRUARY 1979



U.S. Department of Energy

National Solar Heating and
Cooling Demonstration Program

National Solar Data Program

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MONTHLY PERFORMANCE REPORT

STEWART-TEELE-MITCHELL

FEBRUARY 1979

I. SYSTEM DESCRIPTION

The Stewart-Teele-Mitchell site is a single-family residence in Malta, New York. The home has approximately 1900 square feet of conditioned space. Solar energy is used for space heating the home and preheating domestic hot water (DHW). The solar energy system has an array of flat-plate collectors with a gross area of 432 square feet. The array faces south at an angle of 45 degrees to the horizontal. A glycol/water solution is the transfer medium that delivers solar energy from the collector array to a heat exchanger. Water is then used as the transfer medium that delivers solar energy from the heat exchanger to storage, and to the space heating and DHW loads. Solar energy is stored in the basement in a 1000-gallon insulated tank. Preheated city water is stored in a 75-gallon preheat tank and supplied, on demand, to a conventional 40-gallon DHW tank. When solar energy is insufficient to satisfy the space heating load, an oil-fired furnace provides auxiliary energy for space heating. Similarly, an electrical heating element in the DHW tank provides auxiliary energy for water heating. The system, shown schematically in Figure 1, has five modes of solar operation.

Mode 1 - Collector-to-Storage: This mode activates when the collector temperature exceeds the storage temperature by 20°F and terminates when a temperature difference of 3°F is reached. Solar energy is transferred through the heat exchanger that transmits energy from the solar collection loop to the storage loop. Collector loop pump P1 and storage loop pump P2 are operating.

Mode 2 - Collector-to-Space Heating: This mode activates when mode 1 conditions are satisfied and there is a demand for space heating. The collected solar energy bypasses storage and flows directly to the solar heating coil in the air-handling system. Mode diversion valve V2 is open.

Mode 3 - Storage-to-Space Heating: This mode activates when there is a demand for space heating, the temperature at the top of the storage tank exceeds 100°F, and solar energy from the collector is not available. Pump P3 is operating.

Mode 4 - Storage-to-DHW Tank: This mode activates when the temperature at the top of the storage tank exceeds the preheat tank water temperature by 10°F. Pump P4 is operating.

Mode 5 - Summer Mode, Collector-to-Vent: This mode activates when the collector array output fluid temperature exceeds 220°F. The collected solar energy is rejected through a fintube heat exchanger located outside the dwelling. Valve V1 directs the collector loop flow through a purge unit.

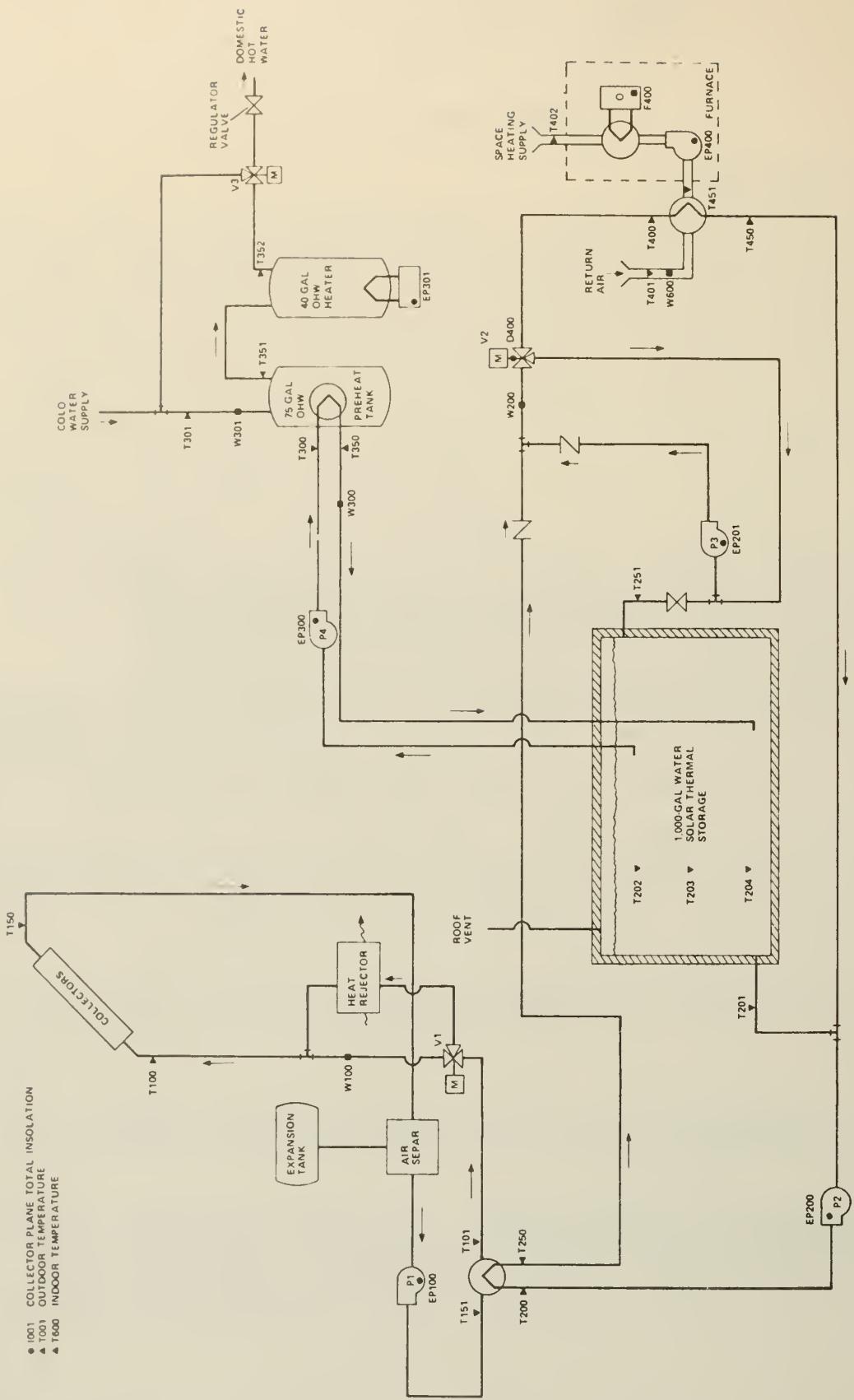


Figure 1. STEWART-TEELE-MITCHELL SOLAR ENERGY SYSTEM SCHEMATIC

II. PERFORMANCE EVALUATION

INTRODUCTION

The solar energy system operated continuously during February. Solar energy satisfied 13 percent of the DHW requirements and 13 percent of the space heating requirements. The solar energy system provided fossil fuel energy savings of 2.2 million Btu at an electrical energy expense of 0.2 million Btu. The collector loop heat transfer fluid appears to have frozen during the period from February 10 through February 15 when temperatures were recorded as low as -19°F. Data was lost for three days in February.

WEATHER CONDITIONS

During the month, total incident solar energy on the collector array was 18.0 million Btu for a daily average of 1485 Btu per square foot. This was above the estimated average daily solar radiation for this geographical area during February of 1131 Btu per square foot for a south-facing plane with a tilt of 45 degrees to the horizontal. The average ambient temperature during February was 13°F as compared with the long-term average for February of 24°F. The number of heating degree-days for the month (based on a 65°F reference) was 1308, as compared with the long-term average of 1162.

THERMAL PERFORMANCE

System - During February the solar energy system performed somewhat poorer than expected. The expected performance was determined from a modified f-chart analysis using measured weather and subsystem loads as inputs. Solar energy collected was 3.5 million Btu versus an estimated 6.1 million Btu. Solar energy used by the system was estimated by assuming that all energy collected would be applied to the load. Actual solar energy used was 1.6 million Btu. System total solar fraction was 13 percent versus an estimated 57 percent.

Collector - The total incident solar radiation on the collector array for the month of February was 18.0 million Btu. During the period the collector loop was operating, the total insolation amounted to 13.6 million Btu. The total collected solar energy for the month of February was 3.5 million Btu, resulting in a collector array efficiency of 19 percent, based on total incident insolation. Solar energy delivered from the collector array to storage was 3.0 million Btu, while solar energy delivered from the collector array directly to the loads amounted to 0.21 million Btu. Energy loss during transfer from the collector array to storage and loads was 0.27 million Btu. This loss represented 8 percent of the energy collected. Operating energy required by the collector loop was 0.13 million Btu.

Storage - Solar energy delivered to storage was 3.0 million Btu and there was no auxiliary energy contribution to storage. There were 1.8 million Btu delivered from storage to the DHW and space heating subsystems. Energy loss from storage was 1.0 million Btu. This loss represented 33 percent of the

energy delivered to storage. The storage efficiency was 67 percent: This is calculated as the ratio of the sum of the energy removed from storage and the change in stored energy, to the energy delivered to storage. The average storage temperature for the month was 88°F.

DHW Load - The DHW subsystem consumed 0.33 million Btu of solar energy and 0.47 million Btu of auxiliary electrical energy to satisfy a hot water load of 0.52 million Btu. The solar fraction of this load was 13 percent. Losses from the DHW subsystem were 0.28 million Btu. The DHW subsystem consumed a total of 0.061 million Btu of operating energy, resulting in an electrical energy savings of 0.016 million Btu. A daily average of 27 gallons of DHW was consumed at an average temperature of 126°F delivered from the tank.

Space Heating Load - The space heating subsystem consumed 1.3 million Btu of solar energy and 8.6 million Btu of auxiliary thermal energy (equivalent to 14.3 auxiliary fossil fuel energy) to satisfy a space heating load of 9.9 million Btu. The solar fraction of this load was 13 percent. The space heating subsystem consumed a total of 0.62 million Btu of operating energy, resulting in an electrical energy expense of 0.058 million Btu.

OBSERVATIONS

During the period from February 10 through February 15, the heat transfer fluid in the collector/heat exchanger loop of the energy collection and storage subsystem (ECCS) appeared to freeze during the night. Temperatures during this period reached nighttime lows between -12°F and -19°F. The days were sunny with daytime temperatures about 6 to 7°F. The scan data shows that the control system normally activated the collector loop pump (EP100), but no flow ensued with the collector inlet temperature (T100) registering 32°F, and the collector outlet temperature (T150) registering as much as 244°F. The temperature at the input to the collector loop heat exchanger (T151) gradually increased to a high of 212°F with the heat exchanger/storage loop pump (EP200) operating normally. The data indicates that a small amount of solar energy was delivered to storage. On February 9 and 10, the heat transfer fluid thawed after approximately three hours of intense insolation, and the flow in the collector/heat exchanger loop was almost normal.

On February 16, the ECSS control system malfunctioned by failing to activate the heat exchanger/storage loop pump (EP200) when the collector/heat exchanger loop was operating.

During February, the measured maximum flow in the collector loop declined by approximately 0.5 gallons per minute since the apparent freezing of the heat transport fluid.

Despite the problems discussed above, the solar energy system registered its best performance of the winter season.

ENERGY SAVINGS

The solar energy system provided a fossil fuel energy savings of 2.2 million Btu at an expense of 0.17 million Btu of electrical energy. The DHW subsystem

provided an electrical energy savings of 0.018 million Btu; the space heating subsystem contributed a fossil fuel energy savings of 2.2 million Btu at an electrical energy expense of 0.06 million Btu.

III. ACTION STATUS

There has been no change in the action status since January. Action on the recommended instrumentation modification and the resolution of sensor anomalies has not been scheduled by Boeing.

SITE: STEWART-TEFLER-MITCHELL
REPORT DATE: FEBRUARY 1970

C-1291-1970-6/6

SOLAR SYSTEM DESCRIPTION:

THE STEWART-TEFLER-MITCHELL SOLAR SYSTEM IS INSTALLED IN A 1200 SQ.FT. CONCRETE FAMILY DWELLING LOCATED IN MANTA, ECUADOR. THE SOLAR SYSTEM USES HOT WATER PREHEATING, HOT WATER CONVENTIONAL HEATING AND HOT WATER CONVENTIONAL HEATING. THE SOLAR SYSTEM IS 40% GLYCOL/WATER. THE SOLAR SYSTEM CAN BE OPERATED IN COOLING FLUID IS WATER. SOLAR ENERGY CAN BE OPERATED IN COOLING OR HOT WATER. THE SYSTEM USES AUXILIARY SPACE HEATING AND HOT WATER, CONCRETE, AIR FLUENCE.

GENERAL SITE DATA:

INVENT SOLAR ENERGY

COLLECTED SOLAR ENERGY

AVERAGE AMBIENT TEMPERATURE
AVERAGE BUILDING TEMPERATURE
FOR SOLAR CONVENTION EFFICIENCY
FOR OPERATING ENERGY
TOTAL SYSTEM OPERATING ENERGY
TOTAL ENERGY CONSUMED

SYSTEM SUMMARY:

	HOT WATER	
SOLAR FACTOR	0.516	0.963
SOLAR ENERGY USE	0.13	0.13
OPERATING ENERGY	0.332	1.311
AUX. THERMAL ENERGY	0.061	0.622
AUX. ELECTRIC ENERGY	0.460	0.552
AUX. FOSSIL FUEL	0.460	0.552
FLERICAL SAVINGS	0.016	14.054
FOSSIL SAVINGS	0.000	-0.055
	2.194	1.94

SYSTEM PERFORMANCE FACTOR:

* DENOTES UNKNOWN DATA

N.A. DENOTES NOT AVAILABLE DATA

PREFERENCE: SOLAR SYSTEM PREFERENCE IS THE MONTAÑA PERFORMANCE REPORT, 1970,

	17.250 MILLION BTU	4.1571 MILLION BTU	2.8476 MILLION BTU	8.0471 MILLION BTU	1.12 MILLION BTU	0.62 MILLION BTU	0.06 MILLION BTU	0.130 MILLION BTU	0.012 MILLION BTU	10.012 MILLION BTU
SYSTEM TOTAL	10.270 MILLION BTU	1.13 PERCENT	1.542 MILLION BTU	1.912 MILLION BTU	0.212 MILLION BTU	0.458 MILLION BTU	0.071 MILLION BTU	0.171 MILLION BTU	0.194 MILLION BTU	10.012 MILLION BTU

SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

MONTHLY REPORT SYSTEM SUMMARY

SITE: STEWART-TEFLER-MITCHELL SOLAR SYSTEM
REPORT PERIOD: FEBRUARY, 1970

SITE/SYSTEM DESCRIPTION:

THE STEWART-TEFLER-MITCHELL SOLAR SYSTEM IS INSTALLED IN A 1000 SQ.FT. STONE FARMHOUSE LOCATED IN MALTA, NY. SOLAR ENERGY IS USED FOR SPACE HEATING AND HOT WATER. THE SYSTEM USES A DIRECT ARRAYS HEAT TRANSFER FLUID IS 40% GLYCOL/WATER. THE STORAGE AND SOLAR ENERGY DISTRIBUTION FLUID IS WATER. SOLAR ENERGY CAN BE DIRECTLY PROVIDED TO THE HOT WATER STORAGE. AIR-TO-LIQUID AIR-TO-FLUID, ENCLOSED

GENERAL SITE DATA:

INCIDENT SOLAR ENERGY

GENERAL	0.446	SOLAR INCIDENCE
47.280	W/SCN	W/SCN
2.055	SOLAR INCIDENCE	SOLAR INCIDENCE
9.596	24/7/365	24/7/365
-1.1	DEGREES F	DEGREES F
0.00	DEGREES F	DEGREES F
0.127	SOLAR INCIDENCE	SOLAR INCIDENCE
0.050	SOLAR INCIDENCE	SOLAR INCIDENCE
0.057	SOLAR INCIDENCE	SOLAR INCIDENCE

AVERAGE AMBIENT TEMPERATURE
AVERAGE BUILDING TEMPERATURE
FROM SOLAR CONVERSION EFFICIENCY
FCCS OPERATING ENERGY
TOTAL SYSTEM OPERATING ENERGY
TOTAL ENERGY CONSUMPTION

SUR SYSTEM SUMMARY:

	HEATING	COOLING
HEAT	0.545	N.A.
SOLAR FRACTION	0.13	N.A.
SOLAR ENERGY USED	0.351	N.A.
OPERATING ENERGY	0.264	N.A.
AUX. THERMAL FNG	0.404	N.A.
AUX. ELECTRIC FUEL	0.404	N.A.
AUX. FUEL SAVINGS	N.A.	N.A.
ELECTRICAL SAVINGS	0.917	N.A.
ENSSIL SAVINGS	N.A.	N.A.

SYSTEM PERFORMANCE FACTOR:

* DENOTES UNAVAILABLE DATA
DENOTES NIL DATA
N.A. DENOTES NOT APPLICABLE DATA
REFERENCE: USE REPORT NUMBER & THE APPROPRIATE PAGES FROM MANUFACTURER'S MANUAL, 1970.

SOLAR/OC4-78

SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

ENERGY COLLECTOR ANALYSIS REPORT (CONTINUED)

SITE: STEWART-TEEL-MITCHELL
RFP/PT DATES: FEBRUARY, 1970

SOLAR / 1-10-76

DAY OF MONTH	INCIDENT SOLAR ENERGY MILLION BTU	AMBIENT TEMP DEG-F	ENERGY TRANS MILLION BTU	PERIODIC PERFORMANCE MULTIPLIER		EFFECTIVE MULTIPLIER	PERIODIC PERFORMANCE MULTIPLIER	EFFECTIVE MULTIPLIER
				DEG-F	DEG-F			
1	0.344	16	0.010	0.002	0.002	0.002	0.002	0.002
2	0.708	15	0.057	0.007	0.007	0.007	0.007	0.007
3	0.902	14	0.116	0.017	0.017	0.017	0.017	0.017
4	0.791	13	0.160	0.026	0.026	0.026	0.026	0.026
5	0.4017	12	0.0000001092	0.0000001092	0.0000001092	0.0000001092	0.0000001092	0.0000001092
6	0.745	12	0.112	0.016	0.016	0.016	0.016	0.016
7	0.145	12	0.0000001092	0.0000001092	0.0000001092	0.0000001092	0.0000001092	0.0000001092
8	0.862	15	0.152	0.024	0.024	0.024	0.024	0.024
9	0.050	15	0.0000001092	0.0000001092	0.0000001092	0.0000001092	0.0000001092	0.0000001092
10	0.960	16	0.047	0.006	0.006	0.006	0.006	0.006
11	0.754	16	0.037	0.005	0.005	0.005	0.005	0.005
12	0.878	16	0.035	0.005	0.005	0.005	0.005	0.005
13	0.965	15	0.043	0.006	0.006	0.006	0.006	0.006
14	0.043	15	0.0000001092	0.0000001092	0.0000001092	0.0000001092	0.0000001092	0.0000001092
15	0.820	16	0.046	0.006	0.006	0.006	0.006	0.006
16	0.971	16	0.049	0.007	0.007	0.007	0.007	0.007
17	*	*	*	*	*	*	*	*
18	*	*	*	*	*	*	*	*
19	*	*	*	*	*	*	*	*
20	0.711	18	0.072	0.006	0.006	0.006	0.006	0.006
21	0.242	20	0.110	0.002	0.002	0.002	0.002	0.002
22	0.411	36	0.062	0.006	0.006	0.006	0.006	0.006
23	0.153	31	0.090	0.007	0.007	0.007	0.007	0.007
24	*	*	*	*	*	*	*	*
25	0.287	30	0.001	0.000	0.000	0.000	0.000	0.000
26	0.000	30	0.002	0.000	0.000	0.000	0.000	0.000
27	0.977	27	0.017	0.001	0.001	0.001	0.001	0.001
28	1.201	32	0.098	0.009	0.009	0.009	0.009	0.009
SUM	17.950	-	2.022	N.A.	0.130	0.162	-	-
Avg	0.641	13	0.072	N.A.	0.005	0.006	0.001	0.001
NRS IN	0001	N/A	0102	N/A	N/A	N/A	N/A	N/A

* DENOTES UNAVAILABLE DATA.

@ DENOTES NILL DATA.

N.A. DENOTES NOT APPLICABLE DATA.

SOLAR HEATING AND COOLING ADMINISTRATION PROGRAM

CONSIDERATION OF THE PROBLEMS OF
THE PRACTICAL APPLICATION OF THE
THEORY OF THE STATE

SITE: STEWART-TEEL-E-MITCHELL
REPORT PERIOD: FEBRUARY, 1970

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* DENOTES UNAVAILABLE APIE DATA.

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N.A. NENTES NNT APPPLICABLF DATA.

SPLASH HEATING AND COOLING DEMONSTRATION

URGENT REPORT
STOPPAGE OF PERFORMANCE

SEPTEMBER 1945: SEPTEMBER, 1944

SPLASH/101A-70/02

DAY OF MONTH	ENERGY TIN STOPPAGE MILLION BTU	ENERGY FDRW STOPPAGE MILLION BTU	CHANCE IN STOPPED ENERGY MILLION BTU	STOPPAGE AVERAGE TEMP DEG F	STOPPAGE EFFICIENCY
1	0.040	0.000	0.018	71	0.600
2	0.220	0.064	0.112	82	0.746
3	0.235	0.095	0.167	84	0.675
4	0.186	0.157	0.122	96	0.777
5	0.080	0.112	0.078	92	0.642
6	0.203	0.072	0.021	94	0.959
7	0.050	0.023	0.022	90	0.722
8	0.143	0.122	0.044	82	0.619
9	0.203	0.154	0.044	77	0.742
10	0.087	0.067	0.022	80	0.322
11	0.067	0.023	0.022	86	0.125
12	0.053	0.025	0.031	84	0.160
13	0.030	0.022	0.022	82	0.250
14	0.160	0.066	0.041	88	0.545
15	0.166	0.067	0.041	88	0.744
16	0.128	0.097	0.021	82	0.327
17	0.227	0.042	0.022	84	0.745
18	*	*	0.023	82	*
19	*	*	0.021	90	1.070
20	0.157	0.070	0.028	92	-0.112
21	0.028	0.102	0.111	82	1.500
22	0.086	0.061	0.068	92	1.0734
23	0.000	0.000	0.005	82	1.000
24	*	*	0.024	82	1.000
25	0.000	0.001	0.010	81	1.000
26	0.000	0.008	0.020	78	1.000
27	0.000	0.017	0.018	78	1.000
28	0.220	0.086	0.160	81	0.362
SUM	2.998	1.814	0.295	-	-
AVG	0.107	0.065	0.007	88	0.673
NRS ID	Q20C	0201	0202	N10A	-

* DENOTES UNAVAILABLE DATA.

? DENOTES NULL DATA

N.O.A. DENOTES NOT APPLICABLE DATA.

SOLAR HEATING AND COOLING DEMONSTRATION PROGRAM

MONTHLY REPORT
HOT WATER SURVEY FORM

SITE: STEWART-TEELF-MITCHELL
REPORT PERIOD: FEBRUARY, 1970

SC LAP/1019-79/02

DAY	HOT WATER LOAD	SOLAR FUEL	SOLAR ENERGY	AUX FUEL	AUX FUEL	FUEL SAVING	FOSSIL ENERGY SAVING	WAT. SAVINGS	HOT WAT. RATE
OF MON.	BTU	BTU	BTU	BTU	BTU	MILLION BTU	MILLION BTU	MILLION BTU	PER GAL
1	0.017	2	0.009	0.017	0.017	0.000	0.000	0.000	27
2	0.026	3	0.020	0.023	0.023	0.000	0.000	0.000	47
3	0.028	4	0.025	0.027	0.027	0.000	0.000	0.000	45
4	0.025	5	0.020	0.024	0.024	0.000	0.000	0.000	48
5	0.029	6	0.021	0.020	0.020	0.000	0.000	0.000	47
6	0.016	7	0.013	0.014	0.014	0.000	0.000	0.000	45
7	0.016	8	0.013	0.016	0.016	0.000	0.000	0.000	24
8	0.020	9	0.020	0.017	0.017	0.000	0.000	0.000	47
9	0.025	10	0.024	0.017	0.017	0.000	0.000	0.000	32
10	0.023	11	0.020	0.017	0.017	0.000	0.000	0.000	47
11	0.023	12	0.025	0.020	0.020	0.000	0.000	0.000	35
12	0.020	13	0.019	0.015	0.015	0.000	0.000	0.000	47
13	0.023	14	0.014	0.017	0.017	0.000	0.000	0.000	17
14	0.025	15	0.013	0.017	0.017	0.000	0.000	0.000	45
15	0.020	16	0.013	0.017	0.017	0.000	0.000	0.000	47
16	0.015	17	0.013	0.017	0.017	0.000	0.000	0.000	56
17	0.015	18	0.013	0.017	0.017	0.000	0.000	0.000	56
18	0.018	19	0.013	0.017	0.017	0.000	0.000	0.000	57
19	0.018	20	0.013	0.017	0.017	0.000	0.000	0.000	57
20	0.020	21	0.013	0.017	0.017	0.000	0.000	0.000	57
21	0.020	22	0.013	0.017	0.017	0.000	0.000	0.000	53
22	0.020	23	0.013	0.017	0.017	0.000	0.000	0.000	22
23	0.020	24	0.013	0.017	0.017	0.000	0.000	0.000	53
24	0.023	25	0.013	0.017	0.017	0.000	0.000	0.000	22
25	0.023	26	0.013	0.017	0.017	0.000	0.000	0.000	53
26	0.022	27	0.013	0.017	0.017	0.000	0.000	0.000	22
27	0.022	28	0.013	0.017	0.017	0.000	0.000	0.000	42
28	0.021	29	0.013	0.017	0.017	0.000	0.000	0.000	24
29	0.021	30	0.013	0.017	0.017	0.000	0.000	0.000	24
30	0.021	31	0.013	0.017	0.017	0.000	0.000	0.000	24
31	0.021	32	0.013	0.017	0.017	0.000	0.000	0.000	24
32	0.021	33	0.013	0.017	0.017	0.000	0.000	0.000	24
33	0.021	34	0.013	0.017	0.017	0.000	0.000	0.000	24
34	0.021	35	0.013	0.017	0.017	0.000	0.000	0.000	24
35	0.021	36	0.013	0.017	0.017	0.000	0.000	0.000	24
36	0.021	37	0.013	0.017	0.017	0.000	0.000	0.000	24
37	0.021	38	0.013	0.017	0.017	0.000	0.000	0.000	24
38	0.021	39	0.013	0.017	0.017	0.000	0.000	0.000	24
39	0.021	40	0.013	0.017	0.017	0.000	0.000	0.000	24
40	0.021	41	0.013	0.017	0.017	0.000	0.000	0.000	24
41	0.021	42	0.013	0.017	0.017	0.000	0.000	0.000	24
42	0.021	43	0.013	0.017	0.017	0.000	0.000	0.000	24
43	0.021	44	0.013	0.017	0.017	0.000	0.000	0.000	24
44	0.021	45	0.013	0.017	0.017	0.000	0.000	0.000	24
45	0.021	46	0.013	0.017	0.017	0.000	0.000	0.000	24
46	0.021	47	0.013	0.017	0.017	0.000	0.000	0.000	24
47	0.021	48	0.013	0.017	0.017	0.000	0.000	0.000	24
48	0.021	49	0.013	0.017	0.017	0.000	0.000	0.000	24
49	0.021	50	0.013	0.017	0.017	0.000	0.000	0.000	24
50	0.021	51	0.013	0.017	0.017	0.000	0.000	0.000	24
51	0.021	52	0.013	0.017	0.017	0.000	0.000	0.000	24
52	0.021	53	0.013	0.017	0.017	0.000	0.000	0.000	24
53	0.021	54	0.013	0.017	0.017	0.000	0.000	0.000	24
54	0.021	55	0.013	0.017	0.017	0.000	0.000	0.000	24
55	0.021	56	0.013	0.017	0.017	0.000	0.000	0.000	24
56	0.021	57	0.013	0.017	0.017	0.000	0.000	0.000	24
57	0.021	58	0.013	0.017	0.017	0.000	0.000	0.000	24
58	0.021	59	0.013	0.017	0.017	0.000	0.000	0.000	24
59	0.021	60	0.013	0.017	0.017	0.000	0.000	0.000	24
60	0.021	61	0.013	0.017	0.017	0.000	0.000	0.000	24
61	0.021	62	0.013	0.017	0.017	0.000	0.000	0.000	24
62	0.021	63	0.013	0.017	0.017	0.000	0.000	0.000	24
63	0.021	64	0.013	0.017	0.017	0.000	0.000	0.000	24
64	0.021	65	0.013	0.017	0.017	0.000	0.000	0.000	24
65	0.021	66	0.013	0.017	0.017	0.000	0.000	0.000	24
66	0.021	67	0.013	0.017	0.017	0.000	0.000	0.000	24
67	0.021	68	0.013	0.017	0.017	0.000	0.000	0.000	24
68	0.021	69	0.013	0.017	0.017	0.000	0.000	0.000	24
69	0.021	70	0.013	0.017	0.017	0.000	0.000	0.000	24
70	0.021	71	0.013	0.017	0.017	0.000	0.000	0.000	24
71	0.021	72	0.013	0.017	0.017	0.000	0.000	0.000	24
72	0.021	73	0.013	0.017	0.017	0.000	0.000	0.000	24
73	0.021	74	0.013	0.017	0.017	0.000	0.000	0.000	24
74	0.021	75	0.013	0.017	0.017	0.000	0.000	0.000	24
75	0.021	76	0.013	0.017	0.017	0.000	0.000	0.000	24
76	0.021	77	0.013	0.017	0.017	0.000	0.000	0.000	24
77	0.021	78	0.013	0.017	0.017	0.000	0.000	0.000	24
78	0.021	79	0.013	0.017	0.017	0.000	0.000	0.000	24
79	0.021	80	0.013	0.017	0.017	0.000	0.000	0.000	24
80	0.021	81	0.013	0.017	0.017	0.000	0.000	0.000	24
81	0.021	82	0.013	0.017	0.017	0.000	0.000	0.000	24
82	0.021	83	0.013	0.017	0.017	0.000	0.000	0.000	24
83	0.021	84	0.013	0.017	0.017	0.000	0.000	0.000	24
84	0.021	85	0.013	0.017	0.017	0.000	0.000	0.000	24
85	0.021	86	0.013	0.017	0.017	0.000	0.000	0.000	24
86	0.021	87	0.013	0.017	0.017	0.000	0.000	0.000	24
87	0.021	88	0.013	0.017	0.017	0.000	0.000	0.000	24
88	0.021	89	0.013	0.017	0.017	0.000	0.000	0.000	24
89	0.021	90	0.013	0.017	0.017	0.000	0.000	0.000	24
90	0.021	91	0.013	0.017	0.017	0.000	0.000	0.000	24
91	0.021	92	0.013	0.017	0.017	0.000	0.000	0.000	24
92	0.021	93	0.013	0.017	0.017	0.000	0.000	0.000	24
93	0.021	94	0.013	0.017	0.017	0.000	0.000	0.000	24
94	0.021	95	0.013	0.017	0.017	0.000	0.000	0.000	24
95	0.021	96	0.013	0.017	0.017	0.000	0.000	0.000	24
96	0.021	97	0.013	0.017	0.017	0.000	0.000	0.000	24
97	0.021	98	0.013	0.017	0.017	0.000	0.000	0.000	24
98	0.021	99	0.013	0.017	0.017	0.000	0.000	0.000	24
99	0.021	100	0.013	0.017	0.017	0.000	0.000	0.000	24
100	0.021	101	0.013	0.017	0.017	0.000	0.000	0.000	24
101	0.021	102	0.013	0.017	0.017	0.000	0.000	0.000	24
102	0.021	103	0.013	0.017	0.017	0.000	0.000	0.000	24
103	0.021	104	0.013	0.017	0.017	0.000	0.000	0.000	24
104	0.021	105	0.013	0.017	0.017	0.000	0.000	0.000	24
105	0.021	106	0.013	0.017	0.017	0.000	0.000	0.000	24
106	0.021	107	0.013	0.017	0.017	0.000	0.000	0.000	24
107	0.021	108	0.013	0.017	0.017	0.000	0.000	0.000	24
108	0.021	109	0.013	0.017	0.017	0.000	0.000	0.000	24
109	0.021	110	0.013	0.017	0.017	0.000	0.000	0.000	24
110	0.021	111	0.013	0.017	0.017	0.000	0.000	0.000	24
111	0.021	112	0.013	0.017	0.017	0.000	0.000	0.000	24
112	0.021	113	0.013	0.017	0.017	0.000	0.000	0.000	24
113	0.021	114	0.013	0.017	0.017	0.000	0.000	0.000	24
114	0.021	115	0.013	0.017	0.017	0.000	0.000	0.000	24
115	0.021	116	0.013	0.017	0.017	0.000	0.000	0.000	24
116	0.021	117	0.013	0.017	0.017	0.000	0.000	0.000	24
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CELLAR HEATING AND COOLING EQUIPMENT

SAFETY MONITORING REPORT

SITE: STEWART-TEELF-MITCHELL
REPORT PERIOD: FEBRUARY, 1970

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* DENOTES UNAVAILABLE DATA.
a DENOTES NULL DATA.
N.A. DENOTES NOT APPLICABLE DATA.

SOLAR HEATING AND CYCLING DEMONSTRATION PROGRAM

ENVIRONMENTAL REPORT

SITE: STEWART-TEEL-MITCHELL
PROJECT NUMBER: EFRQ114P, 1077

SOLAR / 1218-79/67

DAY OF MONTH	TOTAL INSULATION	DIFFUSE INSULATION	AMBIENT TEMPERATURE	RELATIVE HUMIDITY	WIND DIRECTION		WIND SPEED	M.D.H.
					RTV/SN. ET	RTV/SN. ET	DEGREES	DEGREES
1	706	N	16	18	N	NT	-	-
2	1630	NT	16	21	NT	NT	-	-
3	2065	14	21	21	A	A	4	4
4	1622	12	21	21	D	D	0	0
5	1137	16	21	21	D	D	0	0
6	2124	12	16	12	D	D	0	0
7	2326	12	16	12	D	D	0	0
8	1713	16	16	12	NT	NT	0	0
9	1905	16	16	12	NT	NT	0	0
10	1967	16	16	12	NT	NT	0	0
11	12222	1745	15	15	NT	NT	0	0
12	2001	2032	6	6	NT	NT	0	0
13	2182	2182	6	6	NT	NT	0	0
14	1042	1042	6	6	NT	NT	0	0
15	2490	*	1	1	NT	NT	0	0
16	*	*	1	1	NT	NT	0	0
17	*	*	1	1	NT	NT	0	0
18	*	*	1	1	NT	NT	0	0
19	1546	1546	19	19	NT	NT	0	0
20	559	559	20	20	NT	NT	0	0
21	952	952	20	20	NT	NT	0	0
22	355	355	20	20	NT	NT	0	0
23	*	*	20	20	NT	NT	0	0
24	654	654	20	20	NT	NT	0	0
25	220	220	20	20	NT	NT	0	0
26	167	167	20	20	NT	NT	0	0
27	2549	2549	20	20	NT	NT	0	0
28	*	*	20	20	NT	NT	0	0
SUM	41571	N.A.	-	-	-	-	-	-
Avg	1485	N.A.	13	15	N.A.	N.A.	N.A.	N.A.
N.B.	Q001	Q001	N113	N114	N115	N116	N117	N118

* DENOTES UNAVAILABLE DATA.

@ DENOTES NULL DATA.

N.A. DENOTES NOT APPLICABLE DATA.

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